

## Glass transition temperature of thermoplastic starches

M. Mitrus

Food Process Engineering Department, University of Agriculture, Doświadczalna 44, 20-236 Lublin, Poland

Received February 18, 2005; accepted May 4, 2005

**A b s t r a c t.** Thermoplastic starch was produced by mixing potato starch and glycerol in a single screw extruder. The glass transition temperatures of the materials obtained were measured by differential scanning calorimetry (DSC). Both the influence of extruder parameters and material parameters, such as moisture and glycerol content and amyloses/amylopectine ratio were investigated. Repeated extrusion cycles affect the glass transition temperature only to a very small extent.

**K e y w o r d s:** thermoplastic starch, glass transition temperature, differential scanning calorimetry, extrusion

### INTRODUCTION

Over the last decade the increasing amount of refuse and the reduced space for landfill have given rise to an interest in new easily biodegradable materials. Several scientific centers performed research on a special group of natural materials – starch thermoplastics (De Graaf *et al.*, 2003; Myllärinen *et al.*, 2002; Shamekh *et al.*, 2002). To obtain these plastics, starch should be perfectly mixed with a proper quantity of plasticizer to make the material flow at temperatures below the decomposition temperature. In this way it is possible to obtain a product in which the polysaccharides form a continuous, polymeric entangled phase. This form of starch is called thermoplastic starch (TPS) (Van Soest, 1996).

Using the polymer technology designed for synthetic polymers, the starch plastics can be manufactured as a supplement to the existing synthetic products. However, thermoplastic starch is not widely used as a commercial product because of some drawbacks. One of the major problems connected with starchy material is its brittleness. This results from a relatively high glass transition temperature ( $T_g$ ) (De Graaf *et al.*, 2003). The  $T_g$  is a very important parameter for determining the mechanical properties.

For dry starch the  $T_g$  reaches 227°C, whereas with 13% water content a  $T_g$  decrease to 56°C is recorded. The glass transition temperature of gelatinized wheat starch with 22% moisture approximates the ambient temperature (Myllärinen *et al.*, 2002).

The effect of starch plasticized with water addition has been studied frequently just like the comparison of various techniques for glass transition temperature measurement. The method of differential scanning calorimetry (DSC), which is most often used, showed a  $T_g$  that is 10 to 30°C higher than that measured by the nuclear magnetic resonance (NMR) (Myllärinen *et al.*, 2002). The analysis of water influence on the  $T_g$  of amylose and amylopectin proved that branched amylopectin had a slightly lower glass transition temperature than linear amylose.

On the basis of the researches published and of practical observations it can be concluded that starch plastics containing water are brittle under the condition of natural surroundings (Bizot *et al.*, 1997).

The three component systems obtained when starch is plasticized with water and glycerol behave in a more complex way. In research on the influence of glycerol and other plasticizers on the  $T_g$  of potato starch it was found that glycerol plasticizes starch in conformity with Couchman's model that is valid for polymer-solvent combinations (Lourdine *et al.*, 1997). Studies on barley starch plasticized with water and glycerol showed that phase separation is possible and two calorimetric glass transition temperatures can be obtained (Forssell *et al.*, 1997). Moreover, basing on the dielectric-mechanical analysis, the researches where amylose and maltose were plasticized with glycerol showed an increase of the phase separation process together with a decrease of glycerol content below 25%. Only recently, in a study on the behaviour of such two-component systems as

amylose-glycerol, it was found that these systems are composed of phases rich in amylose and phases abounding with glycerol (Moates *et al.*, 2001).

Determination of the glass transition temperature of thermoplastic starch using DSC showed so called 'higher' and 'lower'  $T_g$  values or both simultaneously. The higher and lower  $T_g$ 's are generally found in mixtures containing less than 30% glycerol. This behaviour is likely to be connected with the formation of an area rich in starch and an area rich in glycerol that causes partial phase separation. The higher and lower transitions seem to be characteristics for starch plasticized with glycerol and are independent of the processing method (Forssell *et al.*, 1997).

The tests show that both amylose and amylopectin had a higher  $T_g$ 's in the absence of glycerol. The estimates demonstrated that the  $T_g$  of dry amylose and amylopectin is 227°C, while Bizot *et al.* (1997) assessed the dry starch  $T_g$  as 332°C. What is more, to lower the  $T_g$  of potato starch closer to the ambient temperature, 0.21 g of water should be used for 1g of starch (Bizot *et al.*, 1997; Myllärinen *et al.*, 2002).

Myllärinen *et al.* (2002) confirmed that the  $T_g$  of amylose and amylopectin can be equal to the ambient temperature when the water content is 21%, however at the same glycerol level the  $T_g$  can be still as high as 93°C. It can be concluded that glycerol is a less effective plasticizer than water. On the basis of computations they claim that in order to lower the  $T_g$  value to the ambient temperature, 35% glycerol should be applied.

## MATERIALS AND METHODS

### Materials

Potato starch (Superior Standard) was purchased at the producer, *ie* Food Industry Company 'PEPEES' Stock Company in Łomża (Poland), Potato Company 'Hawa S.A.' in Hława (Poland) and AVEBE Company (the Netherlands).

Glycerol (98.5% purity) originated from the Chemical Plant 'Odczynniki' Ltd in Lublin.

### Determination of amylose in starch

Potentiometric titration with a Pt-electrode and a calomel reference electrode was used. A starch sample with a mass  $m = 200$  mg was dissolved in 10 ml NaOH (5 M). The solution was diluted with water to 100 ml exact. 25 ml of the solution was pipetted to an Erlenmeyer flask, 2 drops of methyl red indicator solution were added and neutralized with HCl (1 M) till it was just red. 1 ml HCl (1 M), 1 ml KI (1 M) and 28 ml NaCl (0.5 M) were added to this solution. The solution was titrated with  $KIO_3$  (0.0050 M =  $t$ ). 1 ml  $KIO_3$  solution corresponds to 0.635 mg  $I_2$ . The potential drop, measured by the potentiometric system (volume  $V$ ), determined the equivalence point and the amylose content can be calculated from (Bates *et al.*, 1943):

$$W(\text{amylose}) = (V t 127 \times 4 \times 5 \times 1000) m^{-1} (\text{mg g}^{-1}).$$

### Blend preparation

Starch and glycerol blends were prepared with a ribbon blender type MPP-100, produced by FMR Rogóźno. The glycerol content varied between 15 and 30 wt %. First, the blends were damped up to the maximum moisture content of 20% based on dry mass. The mixtures were stored in plastic bags for 24 h to intensify glycerin penetration into starch granules. Immediately before the extrusion the blends were remixed (Mitrus, 2004; Mitrus, 2006).

### Granulate extrusion

The extrusion process was conducted at the Department of Process Engineering at the University of Agriculture, Lublin, in a modified single-screw extruder with a screw diameter of 45 mm and a length to diameter ratio of 16/1 (TS-45 produced by ZMCh Metalchem in Gliwice) (Fig. 1). Two dies were used, *ie* one with a single opening of 3 mm diameter and one with a triple opening of 1.5 mm diameter. The extrudate was chopped to granulate of around 5 mm length with a high-speed cutter. From this material films were pressed for testing. The extrusion temperatures ranged from 75 to 140°C, and the screw rotations from 60 to 100 r.p.m. (Mitrus, 2006).



Fig. 1. Single screw extruder TS – 45.

### Differential scanning calorimetry

The measurements of the glass transition temperatures were performed using a Perkin Elmer DSC 7 (Fig. 2) at the Department of Chemical Engineering at the Groningen University in the Netherlands. The thermoplastic starch specimens of 7-10 mg mass were heated from 25 to 180°C at a rate of 10°C min<sup>-1</sup> and then cooled at the same rate to 25°C to be finally reheated to 180°C.

To confirm the obtained results the tests were repeated in a DSC 2920 modulated DSC TA Instruments (Fig. 3). The samples were heated from 0°C up to 150°C at the rate of 1°C min<sup>-1</sup> and then cooled at the same rate to 0°C.

### RESULTS

Figure 4 shows the influence of the blend moisture on the  $T_g$  of potato starch plasticized with 20 and 25% of glycerol. The results show that, in the measured range, moisture of the mixture had only a minimal influence on the  $T_g$  of thermoplastic starch. At 20% glycerol content, a slight decrease of  $T_g$  was observed with an increase of moisture. This is consistent with the scientific reports published in literature. In the case of 25% glycerol level a reverse tendency was noticeable. Together with blend moisture growth, the  $T_g$  value went up as well. However, in those two cases,  $T_g$  value changes were very small and the blend moisture, in measured range, had no significant influence on  $T_g$  changes (Mitrus, 2004).



Fig. 2. Perkin Elmer DSC 7 apparatus.



Fig. 3. Apparatus DSC 2920 modulated DSC TA Instruments.

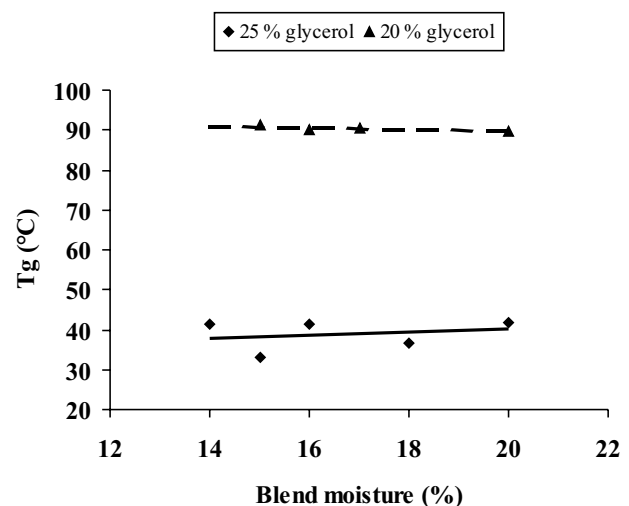


Fig. 4. Influence of blend moisture on the  $T_g$  of thermoplastic starch.

Figure 5 shows the changes of the glass transition temperature with changing glycerol content. The highest  $T_g$  was 132.7°C for 15% of glycerol, and it decreased almost linearly to 18.1°C at a glycerol level of 30%. The moisture content of all the mixtures was 15% (Mitrus, 2004).

Figure 6 illustrates the influence of repeated extrusion on the  $T_g$  of thermoplastic starch for the mixtures with 25% of glycerol. A slight drop of a  $T_g$  can be noted when re-processing thermoplastic starch. The maximum decrease of the glass transition temperature did not exceed 0.15°C. However, it should be mentioned that to avoid thermal destructurization the repeated extrusion experiments were performed at slightly lower temperatures (by around 10°C) (Mitrus, 2004).

Figure 7 illustrates the influence of amylose content on the  $T_g$  of thermoplastic starch for the mixtures with 20% of glycerol. A slight drop of  $T_g$  with amylose content increase was noticed. It is possible that the differences in amylose content in the investigated starches were too low to observe significant differences in  $T_g$  of thermoplastic starch (Mitrus, 2004).

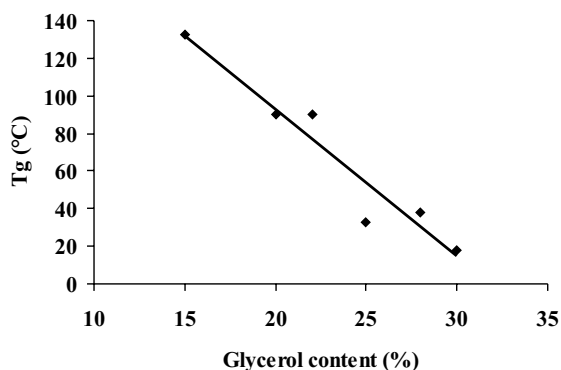


Fig. 5. Influence of the glycerol content on the  $T_g$  of thermoplastic starch.

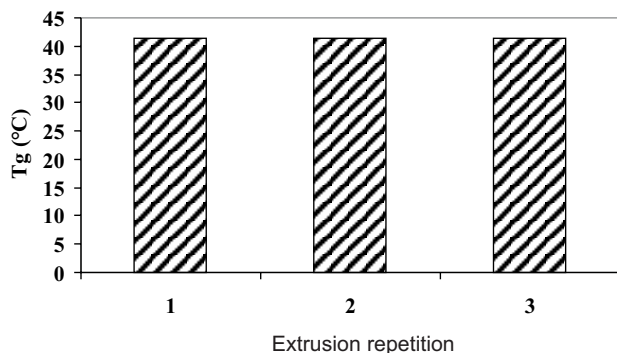


Fig. 6. Influence of multiple extrusions on the  $T_g$  of thermoplastic starch.

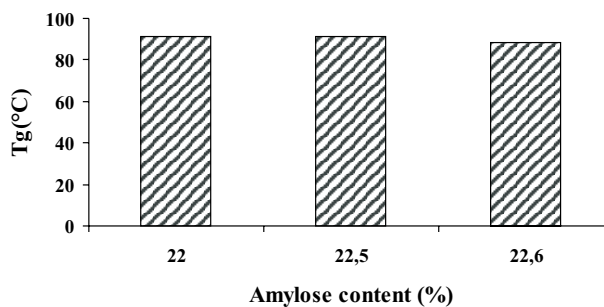


Fig. 7. Influence of amylose content on the  $T_g$  for samples with 20% of glycerol.

## CONCLUSIONS

1. The changes in the glass transition temperature of thermoplastic starch were only minimally affected by the moisture content of the mixture. It was found that, in the measured range, the blend moisture had no significant influence on  $T_g$  changes.

2. When the glycerol content increased from 15 to 30%, the glass transition temperature decreased almost linearly from 132 to 18°C at moisture content of 15%.

3. Multiple extrusion affected the  $T_g$  of potato starch only to a very small degree. A slight downward trend of a  $T_g$  was recorded after multiple re-extrusion, but this did not exceed 0.15°C.

## REFERENCES

- Bates F.L., French D., and Rundle R.E., 1943. Amylose and amylopectin content of starches determined by their iodine complex formation. *J. Amer. Chem. Soc.*, 65, 142-148.
- Bizot H., Le Bail P., Leroux B., Davy J., Roger P., and Buleon A., 1997. Calorimetric evaluation of the glass transition in hydrated, linear and branched polyanhydroglucose compounds. *Carbohydrate Polymers*, 32, 33-50.
- De Graaf R.A., Karman A.P., and Janssen L.P.B.M., 2003. Material properties and glass transition temperatures of differential thermoplastic starches after extrusion processing. *Starch*, 55, 80-86.
- Forsell P.M., Mikkilä J.M., Moates G.K., and Parker R., 1997. Phase and glass transition behaviour of concentrated barley starch-glycerol-water mixtures, a model for thermoplastic starch. *Carbohydrate Polymers*, 34, 275-282.
- Lourdin D., Coignard L., Bizot H., and Colonna P., 1997. Influence of equilibrium relative humidity and plasticizer concentration on the water content and glass transition of starch materials. *Polymer*, 21, 5401-5406.
- Mitrus M., 2004. Influence of barothermal treatment on physical properties of biodegradable starchy biopolymers (in Polish). PhD. Thesis, University of Agriculture, Lublin.
- Mitrus M., 2006. Microstructure of the thermoplastic starch polymers. *Int. Agrophysics*, in press.

- Moates G.K., Noel T.R., Parker R., and Ring S.G., 2001.** Dynamic mechanical and dielectric characterisation of amylose glycerol films. *Carbohydrate Polymers*, 44, 247-253.
- Myllärinen P., Partanen R., Seppälä J., and Forsella P., 2002.** Effect of glycerol on behaviour of amylose and amylopectin films. *Carbohydrate Polymers*, 50, 355-361.
- Shamekh S., Myllärinen P., Poutanen K., and Forsell P., 2002.** Film formation properties of potato starch hydrolysates. *Starch*, 54, 20-24.
- Van Soest J.J.G., 1996.** Starch plastic: structure - property relationships. PhD. Thesis, University of Utrecht, the Netherlands.